

# Critical Aspects Concerning Dynamic Stability of Earthmoving Machines

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Grant: VEGA 1/0198/15

Název grantu: Research of innovative methods for emission reduction of driving units used in transport vehicles and optimisation of active logistic elements in material flows in order to increase their technical level and reliability.

Oborové zaměření: JR Other engineering

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**Abstract:** Dynamic stability of the earthmoving machines is a substantial assumption of their reliable and safe operation. Loss of the stability causes accidents with very serious consequences. There are described in this article the basic theoretical principles concerning the stability theory as well as there are presented two illustrative examples introducing a methodology of the dynamic stability analysis.

**Keywords:** earthmoving machine, wheel loader, dynamic stability, evaluation of dynamic stability, stability failure.

## 1. INTRODUCTION

The stability of machine plays an important role among the most important functional characteristics of the wheeled mobile working machines and the caterpillar mobile working machines, i.e. the earthmoving machines. The stability is a substantial condition with regard to the machine working ability as well as due to a safety of these machines.

There are two main categories of the stability: the static stability and the dynamic stability. The static stability is an ability of the machine to keep its equilibrium position during action of constant external loading. The dynamic stability represents a resistance of the machine to turnover due to external forces that are changing during the current machine operation. The static stability is examined at the machine static position and the dynamic stability is verified during performing of the determined machine working activity.

The consequences of the loss of stability are generally well-known and they do not need to be commented specially, e.g. Fig.1.



Fig. 1 Stability failure during operation of mobile working machine

## 2. DESCRIPTION OF DYNAMIC STABILITY

In order to verify the dynamic stability it is necessary to investigate various variable forces. These forces are defined as the functions of time and functions of the system position. If the system is situated in an equilibrium position in a certain time moment, this situation can be changed suddenly and very quickly just in the next moment. From this reason it is necessary to investigate the system behaviour during action of the various external dynamic negative impacts (failures), i.e. to search a movement of the given system as a whole. Using the mathematical apparatus it is possible to solve this task by means of the corresponding differential equations of motion.

In order to understand the all important phenomena that are connected with the dynamic stability of the mobile working machines, there are presented in the next part of this paper the relevant general definitions from the area of mechanics, which is describing the dynamic equilibrium of a mechanical system. The principle consists in consideration of such situation when the system is shifted from the stable position ( $dx$ ) with a small speed ( $dv$ ). The

stability is kept in such case if the deviation from the previous position remains small.

According to the Fig. 2 it is possible to say that the dynamic equilibrium of the given machine will be kept at that time, as the failures that are disturbing its moving mechanisms cannot cause a loss of contact between the machine and the ground. Let the  $z = z(t)$  is a vertical distance of any point of the machine from the horizontal support. So, it is possible to define the next condition (1): if the vertical acceleration  $\ddot{z}(t)$  of the machine will be less than the acceleration of gravity  $g$ , the machine remains in a stable contact with the ground:

$$\ddot{z}(t) < g \tag{1}$$

or

$$\frac{z_C - z_P + l_2 \cdot \sin \varphi - H \cdot \cos \varphi}{\cos \varphi} - r < 0, \tag{2}$$

where:

$\ddot{z}(t)$  - is the vertical acceleration of the machine ( $m.s^{-2}$ ),

$g$  - is the acceleration of gravity ( $m.s^{-2}$ ),

$z_C = z_C(t)$  - is the vertical coordinate of the gravity centre as a function of time (m),

$z_P = z_P(t)$  - is the coordinate of a path unevenness as a function of time (parameter of failure) (m),

$r$  - is the wheel radius (m),

$\varphi = \varphi(t)$  - is the angle of machine incline as a function of time ( $^\circ$ ),

$H, l_2$  - are the dimensions according to the Fig. 2.

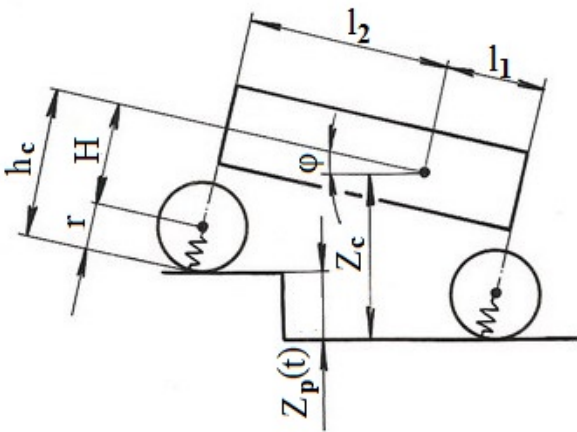


Fig. 2 Dynamic model describing a mobile working machine

In order to determine the conditions (1) a (2) it is necessary to solve the differential equations of the swinging motion or the rollover motion of the machine with regard to the variables ( $z_c; \varphi; \ddot{z}(t)$ ) and to put such obtained values into the relation (2).

The next behaviour of the machine after losing of contact between the machine and the ground depends on the machine dynamic parameters, machine design characteristics and external influences (acting failures). There are two possible scenarios in such case. The first situation is when the machine is able to return back to the basic stable position after an initial deviation. This is the suitable

result of a disturbing situation and it is possible to say in this case that the machine is stable dynamically.

However, the second situation is unfavourable, because in the second case the initial deviation of machine is increasing and the machine is overturning, i.e. the machine is instable dynamically.

So, the decisive factor of stability is a movement tendency of machine after the initial deviation from the original stable position.

According to the [3] there is defined the indicator of stability  $\lambda_t$  by the relation (3), where  $D$  is a set of factors and  $\alpha_R$  is a reserve angle of stability:

$$\lambda_t = \frac{D}{\text{tg } \alpha_R} \tag{3}$$

In order to determine the values  $D$  and  $\lambda_t$  it is necessary to solve the differential equations of the turnover movement. In the Fig. 3 there are illustrated the time behaviours of the function  $\varphi(t)$  for various values of the  $\lambda_t$ .

If  $\lambda_t < 1$ , so the  $\varphi(t)$  values are increasing initially during a certain time  $\tau$  and after this time the  $\varphi(t)$  values are decreasing till to the zero value, i.e. the process is stable.

In the case of  $\lambda_t > 1$  the values of  $\varphi(t)$  are still increasing and the process is instable.

According to the above-mentioned facts it is possible to determine next conditions of the machine dynamic state:

- condition of the dynamic equilibrium:  $\ddot{z}(t) < g$ ,
- condition of the dynamic stability:  $\lambda_t < 1$ ,
- limit of the dynamic stability:  $\ddot{z}(t) = g, \lambda_t = 1$ ,
- condition of the dynamic instability:  $\lambda_t > 1$ .

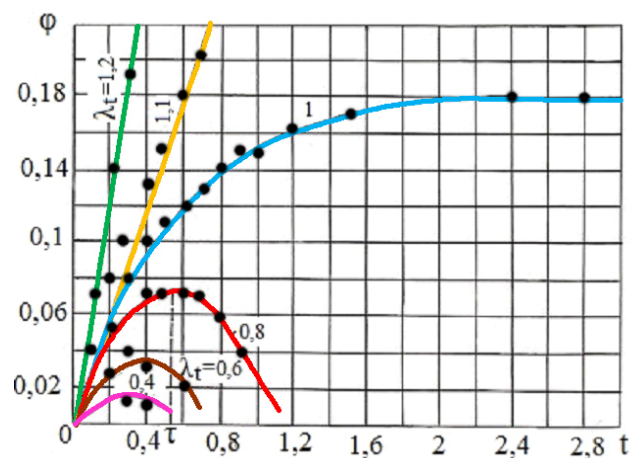


Fig. 3 Time behaviours of the function  $\varphi(t)$  with various values of the  $\lambda_t$

## 2.1 Analysis of the Dynamic Stability

The reserve of stability  $S_\alpha$  can be defined as a ratio of the limit angle of stability  $\alpha_S$  and the real angle of terrain incline  $\alpha$  :

$$S_\alpha = \frac{\alpha_S}{\alpha} = \frac{\alpha_S}{\alpha_S - \alpha_R} \quad (4)$$

whereas  $\alpha = \alpha_S - \alpha_R$  and in the case of the stability condition it should be  $\alpha < \alpha_S$ , i.e. the terrain should be inclined less than is the limit stability angle.

For calculation of the stability reserve can be used also values of the moments or forces. If the  $M_S$  is the stability moment and the  $M_R$  is the reserve moment, so the moment coefficient of the stability  $K_M$  is:

$$K_M = \frac{M_S}{M_S - M_R} = \frac{\sin \alpha_S}{\sin \alpha - \sin \alpha_R} \quad (5)$$

If the  $F_{KL}$  is the force value causing the rollover of machine and the  $Q$  is the real acting force, so the force coefficient of stability is:

$$K_F = \frac{F_{KL}}{Q} \quad (6)$$

The values that are reciprocal to the above-mentioned coefficients of stability are the so-called coefficients of the loading capacity exploitation, i.e. the next ratio values:

$$\gamma_S = \frac{\alpha}{\alpha_S} = \frac{\alpha_S - \alpha_R}{\alpha_S}, \quad \gamma_M = \frac{M_S - M_R}{M_S},$$

$$\gamma_M = \frac{M_S - M_R}{M_S} \quad \text{and} \quad \gamma_F = \frac{Q}{F_{KL}}.$$

For example, for the wheel loaders there is defined the coefficient of stability  $K_F = S_\alpha = 2$  according to the technical standard. This condition means that if the limit angle of the slope is  $20^\circ$ , the permitted angle is only  $10^\circ$ .

The high level of stability reserve applied for the wheeled machines or for machines with the caterpillar chassis is necessary in order to meet the safety requirements also during acting of various dynamic factors.

The minimum value of the stability reserve is:

$$K = \frac{\alpha_S}{\alpha_S - 1,3 \cdot \arctg D} \quad (7)$$

Taking into consideration calculations performed according to the [3] it is possible to say that the loading capacity of the mobile working machines can be increased about 80% on condition that the dynamic stability will be exploited correctly.

### 3. EXAMPLES OF DYNAMIC STABILITY EVALUATION

There are presented in the following part two typical examples of the dynamic stability evaluation in the case of the mobile working machines. The first occurrence is a situation without the machine travelling, Fig. 4 and the second is situation with travelling, Fig. 5. In both cases there is given also the final relation describing the indicator of stability  $\lambda_t$ , which is a dimension-less value according to the [3].

The first case of the dynamic stability investigation without machine travelling enables to realize the stability verification process experimentally using such equipment, which is intended for the static stability testing (e.g. the tilting platform).

The second case requires verification of stability during driving of machine and such experiment is demanding as well as dangerous, but it cannot be performed in laboratory conditions.

#### 3.1 Rapid Stoppage of Jib Sinking

The first possible analysed situation is illustrated on example of a very fast stopping of the jib sinking movement.

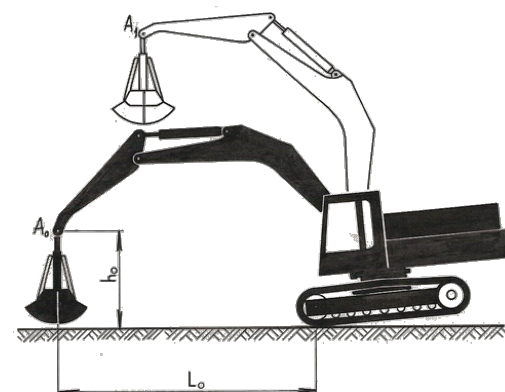


Fig. 4 Dynamic stability of the mobile working machine at the halt

Decision about the dynamic stability is obtained by means of the following two relations:

$$\lambda_t = \frac{C_0 \cdot v \cdot (L_0 \cdot \cos \alpha_0 + h_0 \cdot \sin \alpha_0)}{J \cdot (p^2 + \beta^2) \cdot p} \cdot \frac{1}{\operatorname{tg} \alpha_R}, \quad (8)$$

$$p = \sqrt{\frac{m \cdot g \cdot h_1 \cdot \cos \alpha_R}{J \cdot \cos \alpha_S}}, \quad (9)$$

where is:

$C_0$  – the stiffness of the working equipment reduced to the end of jib, point  $A_0$  ( $\text{N} \cdot \text{m}^{-1}$ ),

$v$  – the speed of the jib lowering ( $\text{m} \cdot \text{s}^{-1}$ ),

$L_0$  – the radius of the jib with regard to the axle of machine rollover (m),

$h_1$  – the height coordinate of the point  $A_1$  (m),

$\alpha_0$  – the degree of the jib rotation ( $^\circ$ ),

$J$  – the moment of inertia of the machine about the axis of rollover ( $\text{kg} \cdot \text{m}^2$ ),

$\beta$  – the natural frequency of the working equipment ( $\text{s}^{-1}$ ).

### 3.2 Wheel Loader Stability in Working Regime

The second demonstrated example represents a sudden stopping of the earthmoving machine during its translation working movement.

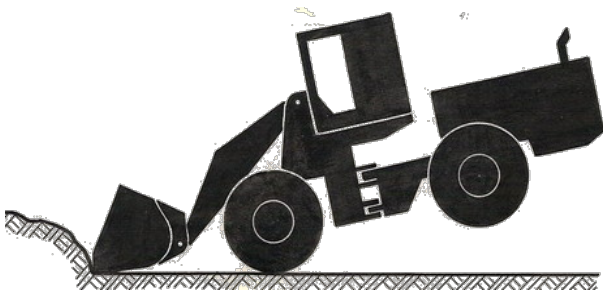


Fig. 5 Dynamic stability of the wheel loader during travelling

The dynamic stability is defined using the next couple of relations:

$$\lambda_t = \frac{C \cdot v_K \cdot h_C}{J \cdot (p^2 + k^2) \cdot p} \cdot \frac{1}{\operatorname{tg} \alpha_R - \frac{F_a - F_V}{m \cdot g}}, \quad (10)$$

$$p = \sqrt{\frac{m \cdot g \cdot h_C \cdot \cos \alpha_R}{J \cdot \cos \alpha_S}}, \quad (11)$$

where is:

$C$  – the reduced stiffness of the system „working equipment - material“ ( $\text{N} \cdot \text{m}^{-1}$ ),

$v_K$  – the speed of machine ( $\text{m} \cdot \text{s}^{-1}$ ),

$F_a$  – the adhesive (pushing) force (N),

$F_V$  – the rolling resistance of the travelling unit (N),

$m \cdot g$  – the total weight of machine (N),

$k$  – the natural frequency of the system „working equipment - material“ ( $\text{s}^{-1}$ ),

$h_C$  – the height coordinate of the machine point of gravity (m),

$J$  – the moment of inertia of the machine about the axis of rollover ( $\text{kg} \cdot \text{m}^2$ ).

## 4. CONCLUSION

Stability of the mobile working machines is always a very relevant question. The static stability and especially the dynamic stability are the most important factors that are influencing the real operational ability of these machines. The question of stability is also a question of the machine safety. From this reason it is necessary to analyse the machine stability state in various working modes or in variable operational situations in order to ensure the safe and reliable working conditions.

This paper was elaborated in the framework of the projects VEGA 1/0198/15 Research of innovative methods for emission reduction of driving units used in transport vehicles and optimisation of active logistic elements in material flows in order to increase their technical level and reliability and KEGA 021TUKE – 4/2015 Development of cognitive activities focused on innovations of educational programs in the engineering branch, building and modernisation of specialised laboratories specified for logistics and intra-operational transport.

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